

MODEL 2008 PULSED OPTICAL FEEDBACK PREAMPLIFIER

The Model 2008 Preamplifier functionally consists of:

- A charge sensitive preamplifier for converting input charge to a proportional output potential.
- Pulse and timing circuits for driving the optical reset stage and the inhibit output.
- Filtering for all power supply lines, and for Detector Bias.

DETAILED CIRCUIT DESCRIPTION

Referring to the functional schematic in Figure 1, the preamplifier section may be analyzed in terms of conventional operational amplifier theory whereby Q101 through Q5 function collectively to provide a large voltage gain, low output impedance and high input impedance. As with any operational amplifier circuit, the voltage gain may be calculated if the source impedance and feedback impedance are known. Therefore, from the test input to the energy output, the calculation is:

$$\text{Ac voltage gain} = (\text{test input divider ratio}) \times \frac{\text{feedback impedance}}{\text{source impedance}}$$

$$A_v = \frac{R_{28}}{R_{28} + R_{26}} \times \frac{C_s}{C_f}$$

In actual operation, the detector converts energy from the radioactive source into a proportional charge while the preamplifier converts this charge into a proportional output potential. The waveforms in Figure 2 illustrate the process by which this occurs.

As the radioactive source emits energy randomly, I_i is instantaneously increased, being equivalent to pulling small increments of charge Q_i from the feedback capacitor C_f . By the well known relationship between voltage and charge,

$$V = \frac{I}{C} \times Q$$

and since by classical feedback theory the op-amp input potential is constrained to be zero,

$$V_o = \frac{I}{C_f} \times Q_i$$

Note, however, that V_o increases with every source emission and that if the circuit is to operate in its linear region, V_o cannot increase without limit. The threshold of comparator A1 sets this upper limit to approximately 2 volts at which point in time the LED (D101) is forced into an ON state.

This LED is placed in such a way so as to illuminate the die of Q101 directly, causing leakage currents to be induced

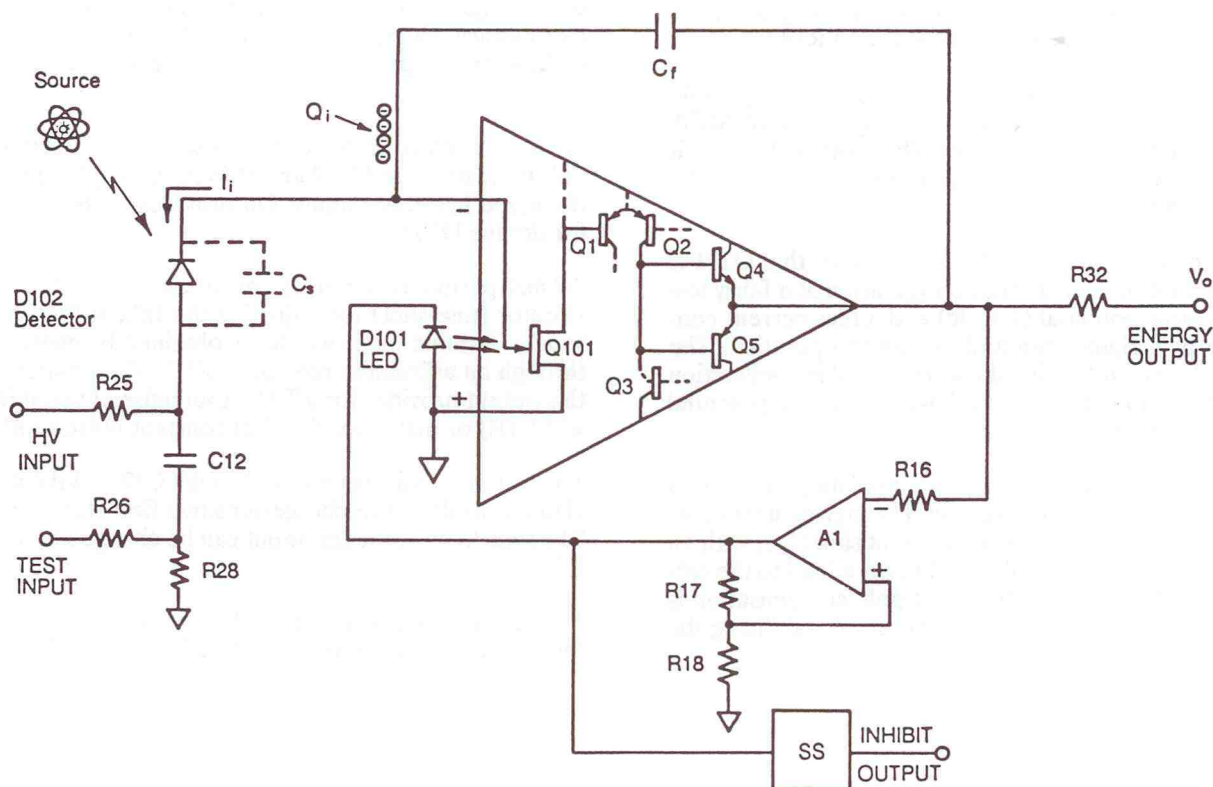


Figure 1 Model 2008 Functional Schematic

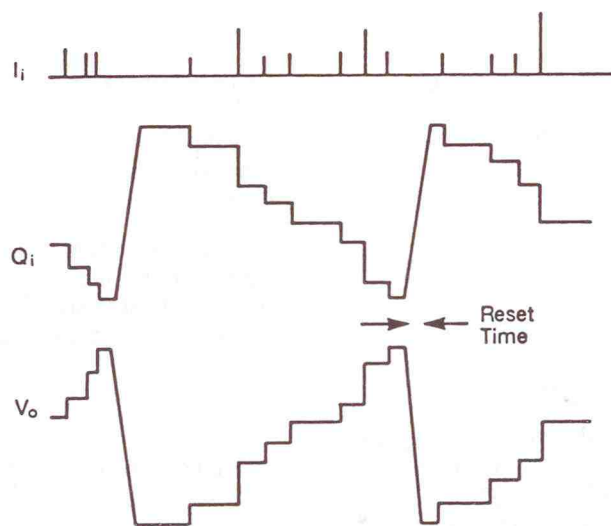


Figure 2 Typical Conversion Waveforms

through the transistor in the opposite direction to those produced by the detector. Thus, the output is forced negatively during this "reset time", but again A1 limits for excursion by extinguishing the LED when the output reaches the new comparator threshold of negative 2 volts. The ability of A1 to change thresholds as a function of its output state is a result of hysteresis introduced by R17 and R18.

Comparator A1 fires a monostable multivibrator to provide an output pulse which can be used to gate off an MCA during the transient following reset. The width of this inhibit pulse is adjustable by means of a screwdriver control on the rear of the 2008.

Referring now to drawing C-17831, it is seen that Q101 is utilized in the common source configuration at a fairly low drain-to-source potential (4 V dc) and a bias current conductive to high signal gain and low noise operation. The resistors RV2 and R4 define this current and in conjunction with R2, R12, and R30, set the base of Q1 at a potential equal to that at the base of Q2.

Q1 and Q2 thus biased form a differential amplifier with a very high non-inverting voltage gain. The high gain is in part a consequence of using an active current sink (Q3) with an output impedance of several megohms as a load to the collector of Q2. At this point dominant pole compensation is provided by C4 and R9 for the purpose of stabilizing the voltage gain over frequency.

Low output impedance drive is accomplished by Q4 and Q5 with R32 acting as a source-to-line matching impedance, insuring pulse fidelity over long cable lengths.

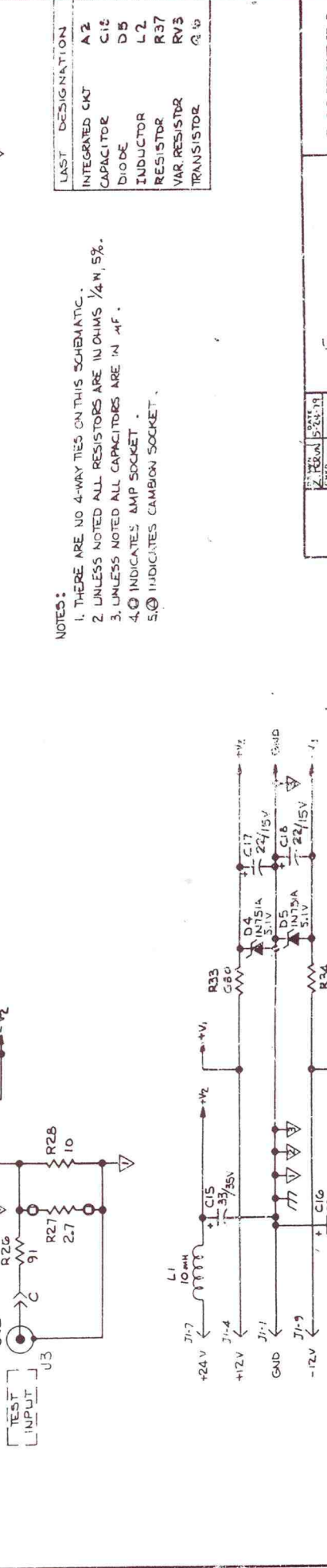
Completing the loop, R14 and R13 send a portion of the output signal back to pin 6 on the cryostat connector. The capacitance which exists between this pin and the gate of Q101 forms the previously mentioned feedback capacitance Cf.

A1 is an open collector comparator with R11 serving as a pull-up resistor and R17 and R18 providing the previously discussed hysteresis limits. Q6 provides current capability for driving D101.

A2 and peripheral circuitry constitute a monostable multivibrator (one-shot) for adjusting the Inhibit Output pulse width. Variable pulse widths are obtained by charging C10 through an adjustable resistance RV3. The jumper plug at this output provides for a TTL-level pulse of variable pulse width (E) or high level signal of constant pulse width (D).

The test input injects change through C12 and the detector element itself to the charge-sensitive first stage amplifier. The sensitivity of the test input can be changed by selecting R27.

The temperature of the input FET, Q101, is optimized at the factory for minimum noise by adjusting RV1.



NOTES:

1. THERE ARE NO 4-WAY TIES ON THIS SCHEMATIC.
2. UNLESS NOTED ALL RESISTORS ARE IN OHMS $\frac{1}{4}$ W, 5%.
3. UNLESS NOTED ALL CAPACITORS ARE IN μ F.
4. \odot INDICATES AMP SOCKET.
5. \odot INDICATES CROCKET SOCKET.

LAST DESIGNATION	A 2	C18	D 5	L 2	R 37	RV 3	Q 10
INTEGRATED CKT							
CAPACITOR							
DIODE							
INDUCTOR							
RESISTOR							
VAR. RESISTOR							
TRANSISTOR							

	SCHMATIC PREAMPLIFIER	MODEL 7008	CANBERRA	B-1793 E
Z KRM 524-19	CHRD	2ND QZCN		
		Q756 IITE		
		W 1000AD 2478		
		FULLY ASS.		

CANBERA

SCHEMATIC
EXAMPLE

15841

WARRANTY

This warranty covers Canberra hardware and software shipped to customers within the United States. For hardware and software shipped outside the United States, a similar warranty is provided by Canberra's local representative.

DOMESTIC WARRANTY

Equipment manufactured by Canberra's Instruments Division, Detector Products Division, and Nuclear Systems Division is warranted against defects in materials and workmanship for one year from the date of shipment.

Canberra warrants proper operation of its software only when used with software and hardware supplied by Canberra and warrants software media to be free from defects for 90 days from the date of shipment.

If defects are discovered within 30 days of the time you receive your order, Canberra will pay transportation costs both ways. After the first 30 days, you will have to pay the transportation costs.

This is the only warranty provided by Canberra; there are no other warranties, expressed or implied. All warranties of merchantability and fitness for an intended purpose are excluded. Canberra shall have no liability for any special, indirect or consequential damages caused by failure of any equipment manufactured by Canberra.

EXCLUSIONS

This warranty does not cover equipment which has been modified without Canberra's written permission or which has been subjected to unusual physical or electrical stress as determined by Canberra's Service Personnel.

Canberra is under no obligation to provide warranty service if adjustment or repair is required because of damage caused by other than ordinary use or if the equipment is serviced or repaired, or if an attempt is made to service or repair the equipment, by other than Canberra personnel without the prior approval of Canberra.

This warranty does not cover detector damage caused by abuse, neutrons, or heavy charged particles.

SHIPPING DAMAGE

Examine shipments carefully when you receive them for evidence of damage caused in transit. If damage is found, notify Canberra and the carrier immediately. Keep all packages, materials and documents, including your freight bill, invoice and packing list. Although Canberra is not responsible for damage sustained in transit, we will be glad to help you in processing your claim.

OUT OF WARRANTY REPAIRS

Any Canberra equipment which is no longer covered by warranty may be returned to Canberra freight prepaid for repair. After the equipment is repaired, it will pass through our normal pre-shipment checkout procedure.

RETURNING EQUIPMENT

Before returning equipment for repair you must contact your Regional Service Center or one of our factories for instructions. For detector repair, contact the Canberra Detector Division in our Meriden, Connecticut, factory for instructions. If you are going to return the equipment to the factory, you must call first to get an Authorized Return Number (ARN).

When you call us, we will be glad to suggest the best way for you to ship the equipment and will expedite the shipment in case it is delayed or lost in transit. Giving you shipping advice does not make us responsible for the equipment while it is in transit.

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DETECTOR SPECIFICATIONS AND PERFORMANCE DATA

Specifications

Model GC1520-7500SL

Serial Number b 95102

The purchase specifications and therefore the warranted performance of this detector are as follows :

Nominal volume cc Relative efficiency 15 %

Resolution 2.0 keV (FWHM) at 1.33 MeV

 keV (FWTM) at 1.33 MeV

1.00 keV (FWHM) at 122 keV

 keV (FWTM) at

Peak/Compton 41 : 1 Cryostat well diameter mm Well depth mm

Cryostat description or Drawing Number if special

Vertical Dipstick, type 7500SL

Physical Characteristics

Geometry Coaxial one open end, closed end facing window

Diameter 51 mm Active volume cc

Length 42 mm Well depth mm

Distance from window 5 mm Well diameter mm

Electrical Characteristics

Depletion voltage (+) 2000 Vdc

Recommended bias voltage Vdc (+) 4000 Vdc

Leakage current at recommended bias .01 nA

Preamplifier test point voltage at recommended voltage -1.3 Vdc

Capacitance at recommended bias —/ pF

Resolution and Efficiency

With amp time constant of 4 μ s

Isotope	^{57}Co	^{60}Co			
Energy (KeV)	122	1332			
FWHM (keV)	.864	1.78			
FWTM (keV)		3.38			
Peak/Compton		50.5:1			
Rel. Efficiency		18.0%			

Tests are performed following IEEE standard test ANSI/IEEE std325-1986

Tested by :

Date : January 19 1995

Approved by :

Date : January 19 1995

Docum : GDAME001
Issue : Spec. Sheet GC
Revue : A
Basis : 0.M001PVE.08

Date : 29/10/93
Name : PVE
Page : 1/1
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